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RESEARCH ARTICLE

MEASUREMENT OF RADON PERMEABILITY THROUGH DIFFERENT MEMBRANE MATERIALS BY USING SURFACE BARRIER DETECTOR (SBD) TECHNIQUE.

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Abstract

The measurement radon permeability through different membrane materials has been carried out by using surface barrier detector (SBD) technique. The permeability constant K and the relative radon permeability $R = n_1/n_2$ for 12 different types of membrane materials (Polyethylene, Cellulose Acetate, Cellulose Nitrate, Polyvinyl Chloride-I, Polyvinyl Chloride-II, Hydrate Cellulose, Polycarbonate, Polyethylene-Terephthalate, Makrofol DE, Makrofol N, Aluminized Polycarbonate and Aluminized Mylar) have been measured. Observed results were found in good agreement with previously reported data for similar membrane materials. The permeability constant for a given commercially available materials vary considerably due to the difference in manufacturing procedures and physical properties of the same material

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Introduction:-

Radon is a radioactive gas that is produced by the decay of uranium. In several studies, it has been confirmed that the inhalation of radon and its progeny is a well-known risk factor for lung cancer at uranium underground miners (Lubin et al., 1994). Radon generated radiations comes in our environment from two major sources (soil and water) by diffusion and transportation processes. The fraction of the radon which escapes depends upon the depth at which it is formed and the permeability of the ground to radon. Radon, being a gas can move from geological environment to human environment through different process; forced or diffusion and convectional flow of fluids in the earth crust. Diffusion of radon in geological and human environment can take place by Graham's law of diffusion. The diffusion of the radon gas through membranes is function of the permeability constant of the membrane materials. In general, the permeability constants for different materials are not widely available in the literature. However, published values (Abdel Fattah et al., 1986; Bigu, 1986; Giridharetal., 1982; Pohl-Ruling et. al., 1980; Ramachandran et.al., 1987; Wojcik, 1991) for a given commercially available material vary considerably due to the difference in manufacturing procedures and physical properties of the same material

In order to measure the radon gas concentration, solid state nuclear track detectors were used. It is extremely sensitive to alpha particles emitted from the two isotopes of the gas ^{222}Rn and ^{220}Rn from their decay products and from any other alpha emitters that may exist near the detector. There are few applications in which special membranes are used to separate radon (^{222}Rn) from thoron (^{220}Rn). The characteristics of these membranes is to delay the diffusion the ^{222}Rn and ^{220}Rn gas (Tanner, 1964). This results a large percentage of the long lived radon i.e. ^{222}Rn will pass through the membrane while a large percentage of the short lived radon i.e. ^{220}Rn will decay during

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its diffusion. In this paper the diffusion of radon gas (^{222}Rn) through different types of membrane has been studied using surface barrier technique. The permeability constant and the relative radon permeability for different types of materials have also been measured.

Experimental Technique

The experimental arrangement for the measurements of radon permeability is shown in the figure 1. It is a radon alpha chamber. The alpha chamber consists of two volumes V_1 and V_2 separately in which V_1 is much larger as compared to V_2 ($V_1 \gg V_2$). The volume V_1 is open and the second volume V_2 is separated from V_1 by a membrane material. A radon source $2.35 \times 10^6 \text{Bq}$ of radium-226 (^{226}Ra) was placed. The numbers of alpha counts n_1 will be taken in the first volume for the measurement of radon concentration after the equilibrium has been reached and the numbers of alpha counts n_2 will be taken in the second volume for the measurement of radon concentration after diffusion through the membrane. The number of alpha counts was measured after the equilibrium has been reached and it is measured in two steps. In the first steps the number of alpha counts n_1 was measured without membrane and in the second steps the number of alpha counts n_2 was measured with the membrane. The method used in the present work is similar to that described by Ramachandran et al. (1987). The significant factor which determines the appropriateness of a membrane for separation radon isotopes is its permeability constant. We define a quantity R which is the ratio of the concentrations of gaseous in volume V_2 with a membrane and the concentration without any membrane in V_1 is expressed by the following relation (Ramachandran et al. 1987):

$$R = n_1/n_2 = \{KA(V_1+V_2)\} / \{KA(V_1+V_2) + V_1V_2\lambda\delta\}$$

Where K is the permeability constant in cm^2s^{-1} , δ is the thickness of the membrane in cm, A is the surface area of the membrane in cm^2 and λ is the decay constant (s^{-1}). The permeability constant is given by the relation:

$$K = \{V_1V_2\lambda\delta / A(V_1+V_2)\} \times \{n_2 / (n_1 - n_2)\}$$

Table 1:- Observed values of radon permeability for different membrane materials

Short Name	Chemical name of the materials	Sample Thickness $\delta(\mu\text{m})$	$R = n_1/n_2$	Permeability Constant ($10^{-12}\text{m}^2\text{s}^{-1}$)
PE	Polyethylene	65	0.45	7.5
CA	Cellulose Acetate	23	0.70	0.65
CN	Cellulose Nitrate	15	0.39	1.9
PVC I	Polyvinyle Chloride	11	0.73	0.50
PVC II	Polyvinyle Chloride	10	0.74	0.63
HC	Hydrate Cellulose	20	0.62	0.95
PC	Polycarbonate	17	0.66	2.2
PET	Polyethylene-Terephthalate	13	0.55	0.29
MAK_DE	Makrofol DE	14	0.40	0.20
MAK_N	Makrofol N	12	0.36	0.40
AP	Aluminized Polycarbonate	35	0.70	0.35
AM	Aluminized Mylar	30	0.60	0.03

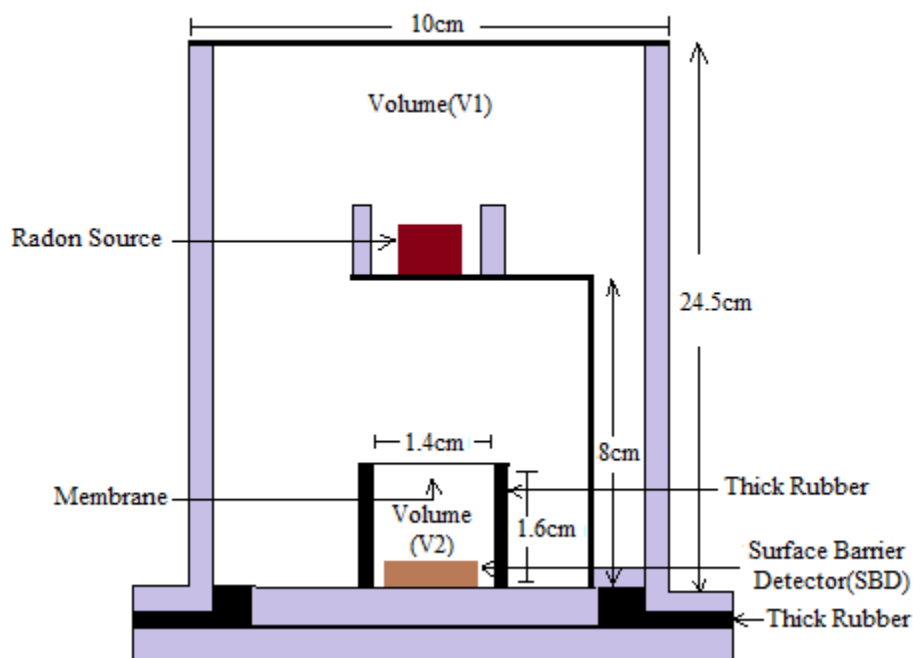


Figure1:-Schematic diagram of the radon alpha chamber.

Result and Discussion:-

The observed permeability constant for different kinds of membrane materials are given in the table 1. These are Polyethylene, Cellulose Acetate, Cellulose Nitrate, Polyvinyl Chloride, Hydrate Cellulose, Polycarbonate, Polycarbonate-Terephthalate, Makrofol, Aluminized Polycarbonate and Aluminized Mylar. In order to obtain an average value of the permeability and ratio n_1/n_2 , the sample were measured several times. The sample area was kept at 3cm^2 in all our measurements. The permeability constant ratio n_1/n_2 for different membrane materials was found respectively $7.5 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.45 for Polyethylene of thickness $65\mu\text{m}$, $0.65 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.70 for cellulose Acetate of thickness $23\mu\text{m}$, $1.9 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.39 for Cellulose Nitrate of thickness $23\mu\text{m}$, $0.50 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.73 for Polyvinyl Chloride I of thickness $11\mu\text{m}$, $0.63 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.74 for Polyvinyl Chloride II of thickness $10\mu\text{m}$, $0.95 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.62 for Hydrate cellulose of thickness $20\mu\text{m}$, $2.2 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.66 for Polycarbonate of thickness $15\mu\text{m}$, $0.29 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.55 for Polyethylene-Terephthalate of thickness $13\mu\text{m}$, $0.20 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.40 for Makrofol DE of thickness $14\mu\text{m}$, $0.40 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.36 for Makrofol N of thickness $12\mu\text{m}$, $0.35 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.70 for Aluminized Polycarbonate of thickness $35\mu\text{m}$ and $0.03 \times 10^{-12}\text{m}^2\text{s}^{-1}$ and 0.60 for Aluminized Mylar of thickness $30\mu\text{m}$. In our observed result an estimated error of about 18% was found. A comparison of our observed results for permeability constant and ratio n_1/n_2 was found good agreement than other values found in the literatures (Ramachandran et al. 1987, Abdel-Fattah et. al. 1986, Giridhar et. al. 1982, Somogyi et. al. 1986).

Conclusions:-

A number of membranes materials of suitable thickness have been used for the measurements of radon permeability. These membrane materials are Polyethylene, Cellulose Acetate, Cellulose Nitrate, Polyvinyl Chloride-I, Polyvinyl Chloride-II, Hydrate Cellulose, Polycarbonate, Polyethylene-Terephthalate, Makrofol DE, Makrofol N, Aluminized Polycarbonate and Aluminized Mylar. The ratio $R = n_1/n_2$ have also been calculated which is the ratio the concentrations of gaseous in volume V_2 with a membrane and the concentration without any membrane in V_1 . This gives the relative permeability through different membrane materials. Our observed result were found good agreement than other values found in the literatures. The permeability constant for a given commercially available materials vary considerably due to the difference in manufacturing procedures and physical properties of the same material

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