

# Cross-Influence of Temperature and Front Layer Thickness on the Performance of a Heterojunction Solar Cell

## Abstract

This study investigates the combined influence of temperature and the thickness of the front surface field (FSF) layer on the electrical performance of a heterojunction solar cell with the structure [(p<sup>+</sup>)-a-Si:H/(n)-c-Si/(n<sup>+</sup>)-a-Si:H]. The analysis is based on numerical simulations performed using the Atlas module of the TCAD SILVACO suite, considering a temperature range from 275 K to 330 K and FSF layer thicknesses varying between 2 nm and 20 nm.

The simulation results reveal a simultaneous degradation of both the open-circuit voltage ( $V_{oc}$ ) and the short-circuit current density ( $J_{sc}$ ) as the temperature increases, particularly in the intermediate FSF thickness range of 3–10 nm. This behavior is primarily attributed to the enhanced carrier recombination at elevated temperatures, especially when the FSF layer is too thin to ensure effective field-induced passivation.

In contrast, thicker FSF layers, specifically those ranging from 13 nm to 20 nm, exhibit improved thermal stability and reduced sensitivity to temperature-induced performance losses. This improvement is likely due to better electric field formation and interface passivation, which mitigate recombination at the a-Si:H/c-Si junction. On the other hand, ultrathin FSF layers (< 5 nm) result in insufficient band bending and weak field-effect passivation, thereby increasing interface recombination and significantly degrading the photovoltaic efficiency.

Overall, the findings underscore the critical role of FSF layer thickness in determining the thermal and optoelectronic behavior of heterojunction solar cells. They highlight the need for simultaneous optimization of the FSF thickness and the cell's thermal operating conditions to ensure stable and efficient performance under realistic environmental variations.

**Keywords:** solar cell, heterojunction, silicon, amorphous silicon, FSF, thickness, temperature, simulation, TCAD-SILVACO

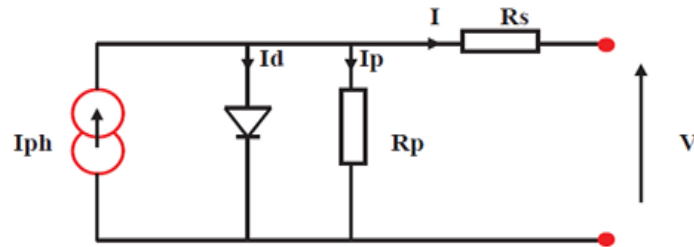
## 30 1. Introduction

31 Silicon-based heterojunction (HJT – Heterojunction with Intrinsic Thin layer) photovoltaic (PV) solar  
32 cells represent a highly promising architecture due to their high efficiency and excellent passivation  
33 properties. This stable technology integrates two types of semiconductor materials, typically arranged  
34 in a trilayer structure forming dual p-n junctions: hydrogenated amorphous silicon / crystalline silicon  
35 / hydrogenated amorphous silicon ( $p^+ \text{-a-Si:H} / n\text{-c-Si} / n^+ \text{-a-Si:H}$ ). The ability to combine amorphous  
36 and crystalline silicon within a single PV device has attracted significant attention over the past  
37 decades and has been the subject of extensive research efforts [1, 2].

38 In this study, we present simulation results focusing on key performance indicators such as the short-  
39 circuit current density ( $J_{sc}$ ), the open-circuit voltage ( $V_{oc}$ ), the fill factor (FF), and the conversion  
40 efficiency ( $\eta$ ) for an HJT solar cell ( $p^+ \text{-a-Si:H} / n\text{-c-Si} / n^+ \text{-a-Si:H}$ ). The simulations are carried out  
41 using the ATLAS module of the TCAD-SILVACO software suite [3], with a particular emphasis on  
42 the influence of temperature variations and the optimization of the front surface field (FSF) layer.

## 43 2. Electrical Modeling of a Solar Cell

44 A photovoltaic solar cell can be modeled by an equivalent electrical circuit consisting of a current  
45 source that represents the incident light power, a diode accounting for the polarization phenomena, a  
46 series resistance representing various contact and interconnection resistances, and a parallel (shunt)  
47 resistance characterizing leakage currents caused by the diode and edge effects at the p–n junction of  
48 the solar cell. The equivalent circuit diagram is shown in Figure 1.



49  
50 Figure 1 : Equivalent Circuit of a Photovoltaic Solar Cell  
51

52 Based on the operating principles of photovoltaic (PV) solar cells and their current–voltage (I–V)  
53 characteristics under illumination, the evaluation of their electrical performance relies on several key  
54 quantities known as photovoltaic parameters [3,4]. The most relevant among them include the fill  
55 factor (FF), open-circuit voltage ( $V_{oc}$ ), short-circuit current density ( $J_{sc}$ ), and power conversion  
56 efficiency ( $\eta$ ).

### 57 Short-Circuit Current ( $I_{sc}$ )

58 The short-circuit current represents the maximum current delivered by a PV solar cell when the  
59 terminal voltage is zero. It is a critical parameter for the characterization of photovoltaic devices. This  
60 current is directly proportional to the intensity of the incident light.

61 Under illumination, the output current at the terminals of the p–n junction constituting the solar cell is  
62 given by the following expression [6,7]:

63 The current–voltage relationship of a photovoltaic solar cell can be described by the following  
64 expression:

$$65 \quad I_L = I_{ph} - I_D - I_{sh} = I_{ph} - I_0 \left[ \exp\left(\frac{q(V + I_L R_s)}{nkT}\right) - 1 \right] - \frac{V + I_L R_s}{R_{sh}} \quad (1)$$

Where:

- 66 • k is the Boltzmann constant,
- 67 • T is the absolute temperature,
- 68 • q is the elementary charge,
- 69 •  $I_{ph}$  is the photocurrent, approximately equal to  $I_{sc}$ ,
- 70 •  $I_0$  is the dark saturation current,
- 71 •  $I_D$  is the diode current,
- 72 •  $I_{sh}$  is the shunt current,
- 73 • V is the output voltage,
- 74 • n is the ideality factor, typically between 1 and 2,
- 75 •  $R_S$  and  $R_{Sh}$  are the series and shunt resistances, respectively.

76 The photocurrent  $I_{ph}$  depends on both irradiance and temperature and is expressed as [8, 9]:

$$I_{ph} = \left( I_{ph_{ref}} + \alpha(T - T_{ref}) \right) \cdot \frac{G}{G_{ref}} \quad (2)$$

77 The saturation current  $I_0$  is given by:

$$I_0 = I_{rs} \left[ \frac{T}{T_{ref}} \right]^3 \exp \left[ \frac{qE_g}{nkT} \left( \frac{T}{T_{ref}} \right) \right] \quad (3)$$

78 With:

$$I_0 = I_{rs} \left[ \frac{T}{T_{ref}} \right]^3 \exp \left[ \frac{qE_g}{nkT} \left( \frac{T}{T_{ref}} \right) \right] \quad (3)$$

$$I_{rs} = \frac{I_{ph}}{\left[ \exp \left( \frac{qV_{oc}}{nkT} \right) - 1 \right]} \quad (4)$$

79 Where  $I_{rs}$  is the diode reverse saturation current.

#### 80 ■ Open-Circuit Voltage ( $V_{oc}$ )

81 The open-circuit voltage, denoted  $V_{oc}$ , is the voltage measured across the terminals of a solar cell  
 82 when the output current is zero ( $I = 0$ ), i.e., when the cell is connected to an infinite load resistance.  
 83 This parameter depends on several factors, including the type of solar cell, the materials used in the  
 84 active layer, the nature of the contact between the active layer and the electrodes, and the illumination  
 85 conditions [5].

86 It is given by the following equation:

$$V_{oc} = \frac{nkT}{q} \cdot \ln \left( \frac{I_{ph}}{I_0} + 1 \right) \quad (6)$$

87 The open-circuit voltage  $V_{oc}$  is proportional to the contact potential difference  $V_D$ , defined as:

$$V_D = \frac{kT}{q} \ln \left( \frac{N_D \cdot N_A}{n_i^2} \right) \quad (7)$$

88 where the intrinsic carrier concentration  $n_i$  is expressed as:

$$n_i = AT^{3/2} \exp \left( -\frac{E_g}{2kT} \right) \quad (8)$$

89 with:

- 90 •  $N_D$ : donor atom concentration,
- 91 •  $N_A$  acceptor atom concentration,
- 92 •  $n_i$ : intrinsic carrier concentration,
- 93 •  $E_g$ : bandgap energy,
- 94 • A: a constant specific to the semiconductor.

95 In Equation (8), the exponential term  $\exp\left(-\frac{E_g}{2kT}\right)$  dominates over the polynomial dependence  $T^{3/2}$ ,  
 96 allowing the variation of  $n_i$  with temperature to be considered essentially exponential.  
 97 As the temperature  $T$  increases, the intrinsic carrier concentration  $n_i$  also increases, leading to a  
 98 decrease in  $V_D$  according to Equation (7), and consequently a reduction in  $V_{oc}$ .

99     ▪ Electrical Power (P)

100 Under standard environmental conditions (illumination, temperature, etc.), the electrical power P (in  
 101 watts) delivered by a photovoltaic cell is defined as the product of the direct current I supplied by the  
 102 cell and the output voltage V [10, 11]:

$$P(W) : U * I$$

103     • **P (W)**: Electrical power measured at the terminals of the PV solar cell.

104     • **U (V)**: Voltage measured across the cell.

105     • **I (A)**: Current delivered by the cell.

106     ▪ Fill Factor (FF)

107 The fill factor is a dimensionless parameter used to evaluate the quality of a photovoltaic solar cell. It  
 108 quantifies the ratio between the maximum power output of the cell and the theoretical power defined  
 109 by the product of the open-circuit voltage and the short-circuit current. It is expressed as:

$$110 \quad \bullet \quad FF = \frac{P_{max}}{V_{oc} \cdot I_{cc}} \quad (9)$$

111     •  $P_{max}$  (W): Maximum power delivered by the cell, corresponding to the operating point  
 112     ( $V_{max}, I_{max}$ ):

$$P_{max} = V_{max} * I_{max}$$

113     •  $V_{max}$ : Voltage at the maximum power point.

114     •  $I_{max}$ : Current at the maximum power point.

115     •  $V_{oc}$  (V): Open-circuit voltage.

116     •  $I_{cc}$  (A): Short-circuit current.

117 The fill factor depends on several factors, including cell design, the quality of the p–n junction, the  
 118 semiconductor material, and the resistivity of the metallic contacts.

119     ▪ Conversion Efficiency ( $\eta$ )

120 The conversion efficiency of a photovoltaic cell is the ratio of the maximum electrical power  $P_{max}$  to  
 121 the incident optical power. It can be improved by increasing the fill factor, the short-circuit current,  
 122 and the open-circuit voltage. The efficiency is defined as:

$$123 \quad \eta = \frac{P_{max}}{P_{inc} \cdot S} = \frac{V_{max} \cdot I_{max}}{P_{inc} \cdot S} = FF \cdot \frac{V_{oc} \cdot I_{cc}}{P_{inc} \cdot S} \quad (10)$$

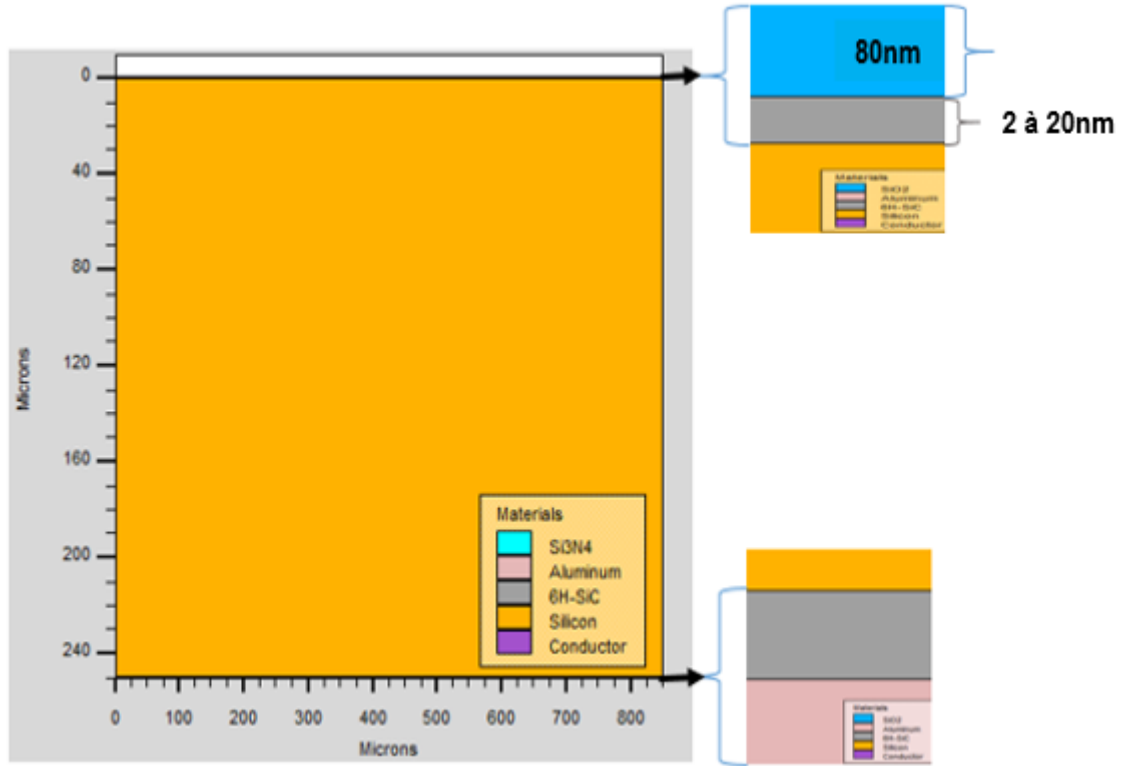
123 where  $P_{inc}$  is the incident power per unit area and S is the surface area of the cell.

124 **3. Matériels, méthodes and Simulation Parameters**

125 The heterojunction solar cell (HJT) is a photovoltaic technology that combines two types of  
 126 semiconductors. Its structure consists of three layers: a crystalline silicon (c-Si) layer acting as the  
 127 active region, sandwiched between two heavily doped hydrogenated amorphous silicon (a-Si:H)  
 128 layers. The front and rear layers serve as the front surface field (FSF) and back surface field (BSF),  
 129 respectively. This multilayer configuration (p<sup>+</sup>)-a-Si:H / (n)-c-Si / (n<sup>+</sup>)-a-Si:H enhances light  
 130 absorption and improves overall energy conversion efficiency.

131 In this work, we investigate the effect of temperature variation on the electrical performance of the  
 132 HJT solar device. The study is carried out using the Atlas simulator from the TCAD SILVACO  
 133 software suite [3]. This 2D/3D device simulator enables predictive modeling of the electrical

134 characteristics of semiconductor components. In addition to external electrical parameters, it provides  
 135 access to internal variables such as electric field distribution and potential profiles.  
 136 These results are obtained by numerically solving Poisson's equation along with the continuity  
 137 equations for electrons and holes over a discretized mesh representing the device structure. Carrier  
 138 recombination mechanisms including Auger and Shockley-Read-Hall (SRH) are also taken into  
 139 account, depending on the doping profile. A schematic representation of a typical HJT cell architecture  
 140 is provided in **Figure 2**.



141  
 142 *Figure 2 : Schematic Structure of the Heterojunction PV Solar Cell to Be Simulated*  
 143  
 144 Simulating the photovoltaic solar cell structure with **TCAD-SILVACO** requires inputting the physical  
 145 parameters of each material layer composing the device.

146 *Table 1: Physical properties of materials used in the simulation*

Different Layers	FSF (a-Si:H)	BSF (a-Si:H)	Substrate (c-Si)	Units
<b>Physical properties</b>				
<b>Thickness</b>	0.1	0.1	250	$\mu\text{m}$
<b><math>E_g</math></b>	1.7	0.7	1.12	eV
<b><math>\chi</math></b>	3.9	3.9	4.05	eV
<b><math>\mu_n</math></b>	$1 \cdot 10^{-6}$	$1 \cdot 10^{-6}$	$1 \cdot 10^{-3}$	$\text{cm}^{-2}/\text{V} \cdot \text{s}$
<b><math>\mu_p</math></b>	$1 \cdot 10^{-6}$	$1 \cdot 10^{-6}$	$1 \cdot 10^{-3}$	$\text{cm}^{-2}/\text{V} \cdot \text{s}$
<b><math>N_c</math></b>	$2 \cdot 10^{20}$	$2 \cdot 10^{20}$	$2.8 \cdot 10^{19}$	$\text{cm}^{-3}$
<b><math>N_v</math></b>	$2 \cdot 10^{20}$	$2 \cdot 10^{20}$	$1.04 \cdot 10^{19}$	$\text{cm}^{-3}$
<b><math>\epsilon</math></b>	11.9	11.9	11.9	F/cm

147  
 148  $E_g$  : energy bandgap  
 149  $\chi$  : electron affinity

150  $\mu_n, \mu_p$  : electron and hole mobilities  
 151  $N_c, N_v$  : effective density of states in the conduction and valence bands  
 152  $\epsilon$  : relative permittivity  
 153 The defect states present in the thin hydrogenated amorphous silicon layers (notably in the BSF, and  
 154 variably in the FSF) are characterized by the parameters listed in the following table.

155 *Table 1 : Simulation parameters for defect state densities and capture cross-sections*

Defect parameters	Acceptor defects (A)	Donor defects (D)	Units
$N_{GA}, N_{GD}$	$1,5 \cdot 10^{15}$	$1,5 \cdot 10^{15}$	$\text{cm}^{-3}$
$N_{TA}, N_{TD}$	$1 \cdot 10^{21}$	$1 \cdot 10^{21}$	$\text{cm}^{-3}$
$E_{GA}, E_{GD}$	0,62	0.78	eV
$W_{GA}, W_{GD}$	0,15	0.15	eV
$W_{TA}, W_{TD}$	0.033	0.049	eV
$\sigma_n$	$1 \cdot 10^{-17}$	$1 \cdot 10^{-15}$	$\text{cm}^{-2}$
$\sigma_p$	$1 \cdot 10^{-15}$	$1 \cdot 10^{-17}$	$\text{cm}^{-2}$

156  
 157  $N_{GA}, N_{GD}$  : Gaussian-shaped acceptor/donor defect densities  
 158  $N_{TA}, N_{TD}$  : Tail state densities near the conduction/valence bands  
 159  $E_{GA}, E_{GD}$  : Energy position of the Gaussian peak  
 160  $W_{GA}, W_{GD}$  : Width of the defect energy distribution  
 161  $W_{TA}, W_{TD}$  : Largeur de la distribution  
 162  $\sigma_n, \sigma_p$  : Electron and hole capture cross-sections  
 163 All simulations were conducted under standard test conditions: AM1.5 spectrum, 0.1 W/cm<sup>2</sup>  
 164 irradiance, and a temperature of 300 K.

## 165 4. Results and Discussion

166 Photovoltaic solar cells are optoelectronic devices capable of converting solar energy directly into  
 167 electrical energy. Designed for outdoor use, these cells are exposed to significant temperature  
 168 variations, ranging from early morning cold to peak sunlight heat, depending on their location.  
 169 Therefore, understanding their electrical behavior across a wide temperature range is essential.  
 170 In this study, we examine the effect of temperature variation (from 275 K to 330 K) on the main  
 171 electrical performance parameters of a heterojunction solar cell, including voltage, power, current  
 172 density, fill factor, and efficiency. The analysis is performed using the Atlas simulator from the  
 173 TCAD-SILVACO software suite.

### 174 4.1. Temperature Effect on Conversion Efficiency ( $\eta$ ).

175 Figure 3 illustrates the variation in conversion efficiency of the heterojunction solar cell as a function  
 176 of temperature, for different thicknesses of the FSF layer.

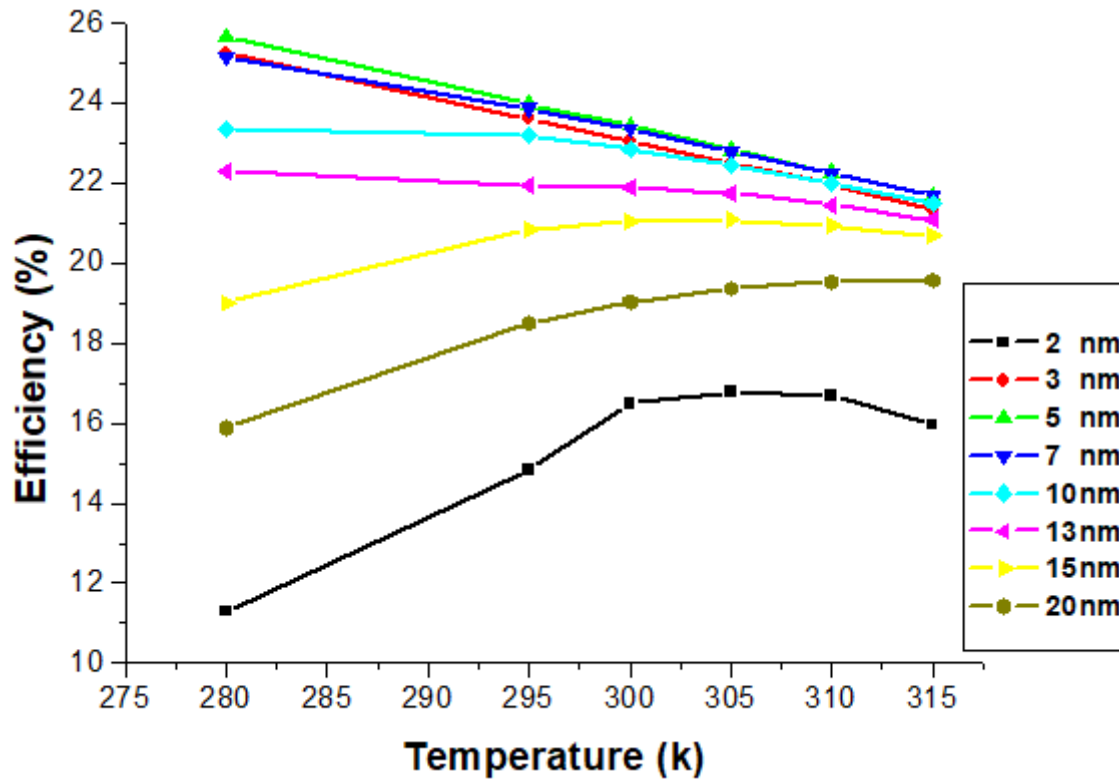


Figure 3 : Efficiency Evolution of a Cell with Varying FSF Layer Thicknesses as a Function of Temperature

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180 Simulation results show that for photovoltaic solar cells with FSF layer thicknesses ranging from 3 nm  
181 to 10 nm, the conversion efficiency ( $\eta$ ) exhibits a significant decline as the temperature increases from  
182 275 K to 330 K. In contrast, for FSF thicknesses between 13 nm and 15 nm, the efficiency improves  
183 steadily with temperature up to 300 K, followed by a slight decrease or stabilization. A specific trend  
184 is also observed for cells with 2 nm and 20 nm thick FSF layers, which show a slight increase in  
185 efficiency within the same temperature range.

186 The pronounced efficiency drop in the 3–10 nm range can be attributed to the enhanced thermal  
187 agitation of free charge carriers, leading to a reduction in diffusion length and an increase in non-  
188 radiative recombination rates. Thin FSF layers are more prone to localized thermal accumulation,  
189 which limits charge collection and reduces performance at elevated temperatures [12].

190 Conversely, the improvement in efficiency observed for the 20 nm FSF layer is explained by a longer  
191 diffusion length that benefits from thermal activation. In this case, carriers that previously struggled to  
192 traverse the space-charge region due to insufficient diffusion are assisted by thermal energy, resulting  
193 in improved separation and collection that partially compensates for recombination losses.

194 The efficiency curve also highlights a significant performance drop when the front a-Si:H layer is  
195 reduced to an ultrathin thickness of 2 nm. Contrary to explanations based on excessive optical  
196 transparency, this drop is more accurately attributed to poor passivation of the crystalline silicon  
197 surface. As demonstrated by Bivour et al. (2012) [13], when the a-Si:H layer thickness falls below 5  
198 nm, the passivation quality at the a-Si:H/c-Si interface degrades significantly, leading to increased  
199 surface recombination and reduced efficiency.

200 This observation is supported by Taguchi et al. (1994) [14], who showed that optimal passivation  
201 using a-Si:H is a critical factor for achieving high-efficiency heterojunction cells. The deposition of an

202 ultrathin front layer compromises both junction formation and surface passivation, leading to a sharp  
203 increase in recombination losses.

204 An optimized front layer thickness thus provides a necessary balance between effective electronic  
205 passivation and sufficient optical transparency, ensuring efficient photocarrier collection and enhanced  
206 photovoltaic performance.

207 In addition, the efficiency curve reveals a progressive improvement in cell performance between 270  
208 K and 300 K, followed by a plateau. This behavior may be attributed to increased thermal agitation,  
209 which facilitates the release of charge carriers trapped in shallow energy states, temporarily reducing  
210 recombination losses and enhancing the overall conversion efficiency.

#### 211 **4.2.Effect of Temperature on the Short-Circuit Current Density ( $J_{sc}$ )**

212 The current density generated by a solar cell results from the sum of the diffusion current densities of  
213 electrons and holes, along with the dominant generation current in the depletion region. It can be  
214 expressed by the following relation:

$$J = J_p + J_s = J_s \left[ \exp\left(\frac{qV}{KT}\right) - 1 \right] = \left( \frac{qD_p p_{n0}}{L_p} + \frac{qD_n n_{p0}}{L_n} \right) \left[ \exp\left(\frac{qV}{KT} - 1\right) \right] \quad (11)$$

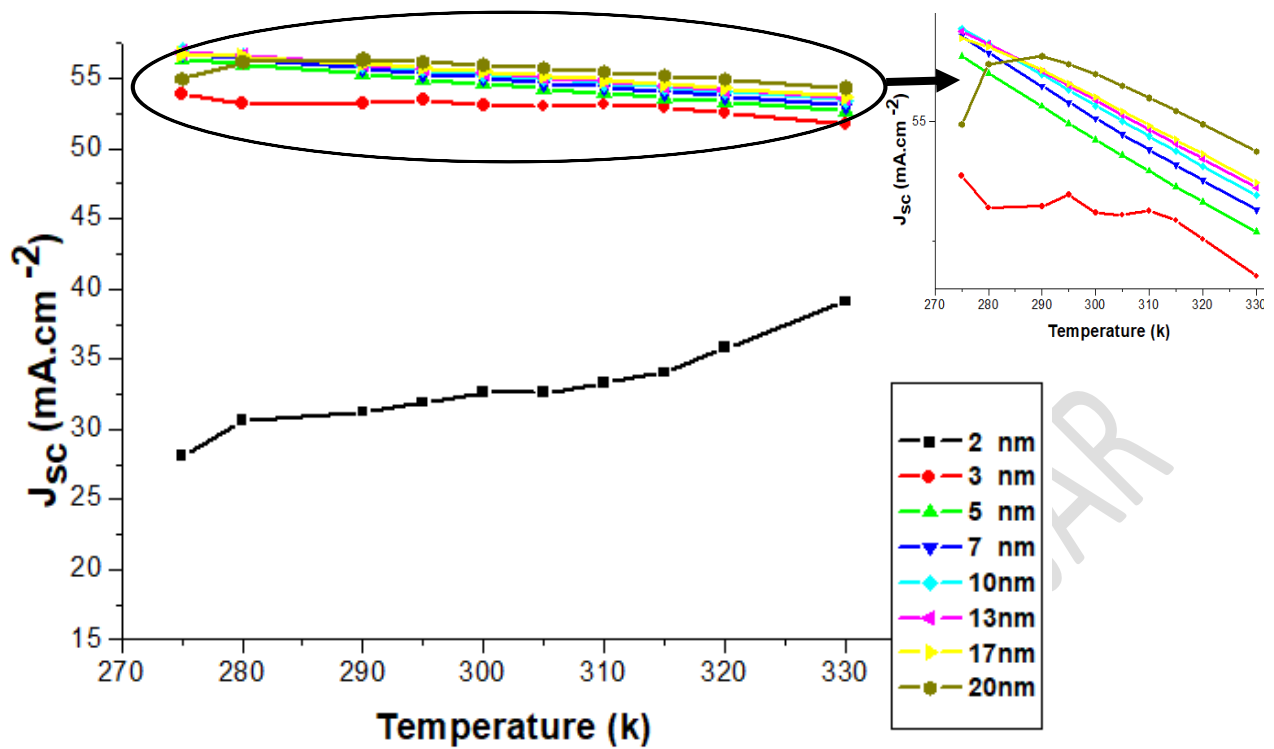
215 where:

- 216 •  $J_s$  is the saturation current density,
- 217 •  $D_n$  and  $D_p$  are the diffusion coefficients of electrons and holes, respectively,
- 218 •  $L_n = \sqrt{D_n \tau}$  and  $L_p = \sqrt{D_p \tau}$  are the corresponding diffusion lengths,
- 219 •  $n_{p0}$  and  $p_{n0}$  represent the minority carrier concentrations in the p-type and n-type regions,

220 This equation clearly shows that the current density is inversely affected by temperature. As  
221 temperature increases, the thermal agitation of charge carriers intensifies, which disrupts carrier  
222 transport and reduces their collection efficiency—ultimately leading to a decrease in short-circuit  
223 current density.

224 Figure 4 illustrates the evolution of the current density in a heterojunction solar cell as a function of  
225 temperature, for various FSF layer thicknesses.





226

227 *Figure 4 : Evolution of Current Density as a Function of Temperature for Various FSF Layer Thicknesses*

228

229 The results presented in Figure 4 reveal a quasi-linear decrease in current density as the temperature  
 230 increases. This trend is consistent with the theoretical expression that relates current density, voltage,  
 231 and temperature, as established in (11).

232 Furthermore, the observed variation strongly depends on the thickness of the emitter layer (FSF). For  
 233 thicknesses between 5 nm and 20 nm, the current density decreases in a gradual and relatively uniform  
 234 manner with temperature. In contrast, for a cell with an FSF layer of 3 nm, the current density remains  
 235 almost constant, despite the rise in temperature indicating apparent thermal stability for this  
 236 configuration.

237 However, when the FSF thickness drops below 3 nm, a noticeable performance degradation is  
 238 observed. This is attributed to a significant deterioration in the passivation quality of the a-Si:H / c-Si  
 239 interface, which leads to increased non-radiative recombination. As a result, the current density  
 240 decreases due to less efficient collection of photogenerated carriers.

#### 241 **Effect of Temperature on the Fill Factor (FF)**

242 Figure 5 illustrates the variation of the fill factor (FF) of a heterojunction solar cell as a function of  
 243 temperature, for different FSF layer thicknesses. This analysis provides insight into how temperature  
 244 affects the quality of the maximum power point, and therefore the overall performance of the device.

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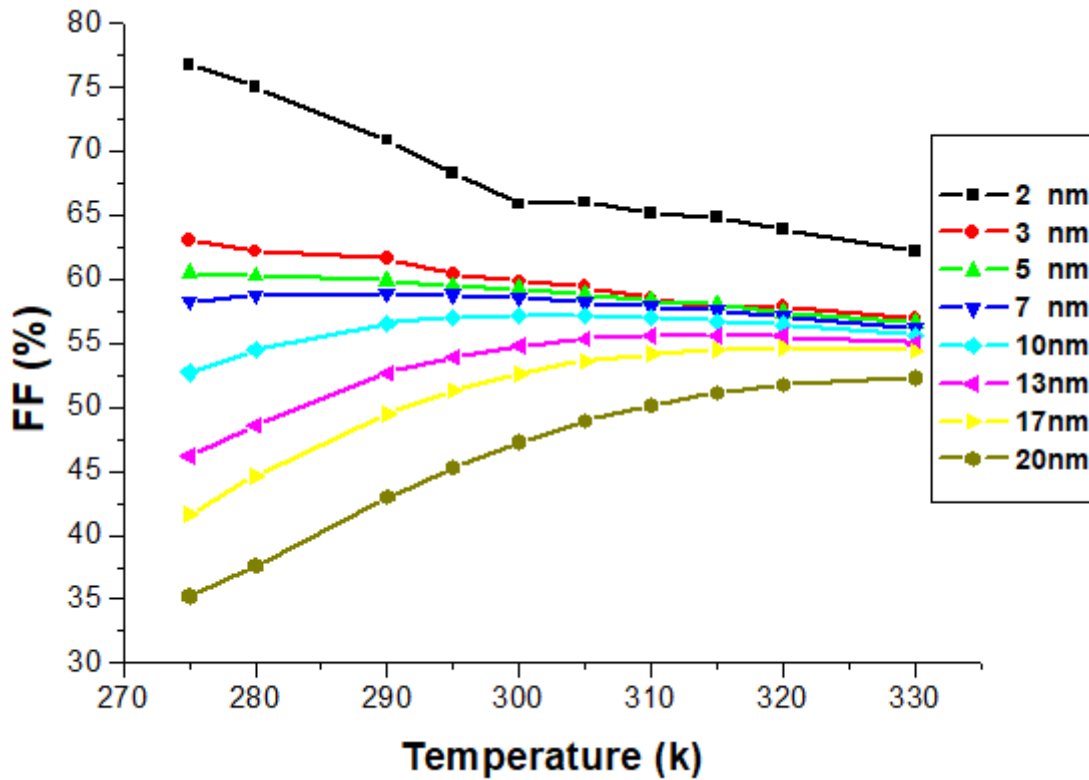


Figure 5 : Evolution of the Fill Factor of a Photovoltaic Cell as a Function of Temperature for Different FSF Layer Thicknesses

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The analysis of Figure 5 reveals distinct trends in the evolution of the fill factor (FF) with temperature, depending on the FSF layer thickness:

- A decrease in FF is observed for photovoltaic cells with FSF thicknesses of 3 nm and 5 nm;
- A stabilization of FF is seen for thicknesses of 7 nm and 10 nm;
- A progressive improvement in FF is noted for FSF layers between 13 nm and 20 nm.

The reduction in fill factor for thinner layers is primarily due to the combined effect of decreasing output voltage and increasing series resistance within the cell. Thermal agitation, induced by the temperature rise in thin layers, increases resistivity, which deteriorates the internal transport conditions and lowers the FF.

Conversely, the improvement observed for thicker FSF layers is attributed to a decrease in effective resistivity, resulting from a reduction in bulk recombination. This leads to more efficient carrier extraction and an enhancement of the maximum power point.

#### 4.3.Effect of Temperature on Open-Circuit Voltage ( $V_{oc}$ )

Figure 6 illustrates the variation of open-circuit voltage ( $V_{oc}$ ) in a heterojunction solar cell as a function of temperature, for various FSF layer thicknesses. The observed behavior is consistent with findings reported in previous studies [2, 16, 17, 18].

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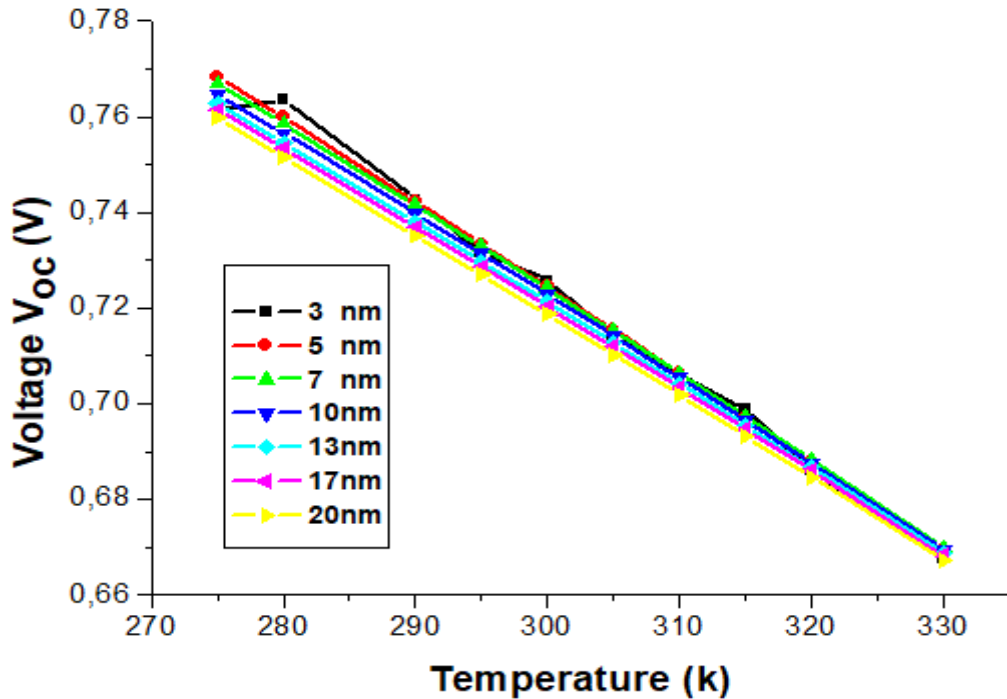


Figure 6 : Variation of Open-Circuit Voltage with Temperature for Different FSF Layer Thicknesses

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269 The analysis of Figure 6 highlights the significant negative impact of temperature on the open-circuit  
 270 voltage ( $V_{oc}$ ). A linear decrease in  $V_{oc}$  is observed as temperature increases. This decline is attributed  
 271 to the enhanced thermal agitation of atoms in the semiconductor material, which leads to an increase in  
 272 the reverse saturation current ( $I_0$ ).

273 According to Equation (3),  $I_0$  which is linked to thermally activated charge carrier recombination rises  
 274 rapidly with temperature. As described by Equation (6), this results in a steady decline in open-circuit  
 275 voltage. These findings are consistent with previous theoretical and experimental studies, which report  
 276 that the efficiency of photovoltaic cells decreases with rising temperature [18, 19, 20, 21].

277 Thus, as the temperature increases, the open-circuit voltage of the solar cell decreases, leading  
 278 consequently to a drop in energy conversion efficiency.

## 279 5. Conclusion

280 The influence of temperature on a heterojunction solar cell with the structure (p<sup>+</sup>)-a-Si:H / (n)-c-Si /  
 281 (n<sup>+</sup>)-a-Si:H has been investigated using the Atlas simulator from the TCAD-SILVACO software suite.  
 282 The study focused on photovoltaic cells with varying FSF layer thicknesses.

283 The results confirm a negative temperature effect on key performance parameters such as the open-  
 284 circuit voltage ( $V_{oc}$ ) and short-circuit current density ( $J_{sc}$ ), particularly in cells with thin front layers.  
 285 However, improvements in both efficiency and fill factor were observed for cells with a 20 nm FSF  
 286 layer, suggesting better thermal stability in those configurations.

287 These findings emphasize the importance of considering local climatic conditions, especially  
 288 temperature variations, when designing and optimizing heterojunction solar cells for real-world  
 289 applications.

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